Effect of Different Designs of Drip Irrigation system on Maize Productivity in Reclaimed Lands

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ABSTRACT
Drip irrigation systems consider as the most efficient of water distribution and application and an ideal way for supplying the plants with nutrients. It demonstrated a superior performance under desert conditions for sandy soils. Two field experiments were conducted in two seasons, at the experimental farm of National Research Centre (NRC), El-Nubaria, Beheira Governorate to investigate the effect of drip irrigation designs on Maize (Zea mays L., single cross 10 hybrid) production under reclaimed lands. Four different lateral designs as (double inlet, loop tube, flushing pipe, and single inlet) were tested under surface and subsurface drip irrigation systems. Results indicated that the lowest percentage of pressure drop was 6.4 and 6.6 % that recorded for the double inlet design under both sub-surface and surface drip irrigation systems SSDI, SDI respectively. The highest percentage of pressure drop was 12.3 and 9.8 % that recorded for the single inlet design of surface and sub-surface systems respectively. The higher emission uniformity, crop yield, and water use efficiency were recorded for the double inlet design under sub-surface drip irrigation system 96.34%, 11.86 t / ha, and 1.699 kg m⁻³ comparing with single inlet design which were 90.76 %, 9.07 t / ha, and 1.344 kg m⁻³ under surface drip irrigation system, respectively. The statistical analysis shown a significant differences at the 5% level in both maize yield and water use efficiency between treatments. Generally, (Hydraulic performance, Emission uniformity, Crop yield, and Water use efficiency) were higher in closed designs SSDI, SDI and sub-surface system comparing with single inlet design and the surface drip irrigation system.

Keywords: Maize, drip irrigation, double inlet, single inlet, and design.

1. Introduction
Drip irrigation has become widespread in the world due to water scarcity concerns in many parts of the world (Sahin et al., 2005). Drip irrigation system is traditionally the application of a constant steady flow of water to soil at low pressure. In this system, water is applied directly to the root zone of plants by means of applicators (drippers) operated under low pressure with the applicators being placed either on or below the surface of the ground. Water loss is minimized through these measures, as there is very little splash owing to the low pressure and short distance to the ground (Ali, 2011). Subsurface drip irrigation (SSDI) is known as one of the most effective irrigation methods capable in improving (WUE) through providing small amounts of water at short irrigation intervals and causing little or no water loss in terms of deep percolation, run-off and soil evaporation, resulting in improved water and nutrient uptake by plants and enhanced (WUE) (Nermin, 2015). Subsurface drip irrigation saves water, improves crop yields and quality, and facilitates fertilizer application; however, system performance is dependent upon skilled management (Waller and Yitayew, 2016). It is characterized by a high efficient water use due to the reduction or elimination of soil water evaporation, surface run-off, and deep percolation (Lamm and Camp, 2007).

Pressure drop occurs due to water flowing through pipes, fittings, and other components of the irrigation system. The magnitude of this energy loss depends on the velocity of the flowing water, the
“roughness” of the flow path through pipes, fittings, and components, and the number of flow directional changes through fittings and components. In addition, excessive energy losses within mainlines, sub-mains, header, and/or lateral pipe sections can result in substantial variations in operating pressure and non-uniform application of water throughout the hydraulic network (Clark et al., 2007). The pressure drop in built-in lateral tubes is affected by the flow average velocity, emitter spacing, and pipe inside diameter, emitter inside diameter and emitter length (Imam et al., 2015). Distributed uniformity of water and nutrients along the laterals in traditional trickle irrigation systems are negatively affected with large reduction in pressure at the ends of laterals. Accordingly, a reduction in plant growth and yield follow the same trend (Mansour, 2016).

Better performances in terms of power consumptions, emission uniformities, savings of power and water, lower ranges in pressure regulations, pressure balancing and other associated parameters can be achieved in the multi-loop type piping systems as compared to the similar type of multilateral piping drip irrigation systems (Dhara, 2014). The mean uniformity in the proposed looped with carrier network is higher than the traditional network. The pressure distribution along the laterals in the looped with carrier network is better than that in the traditional and looped network. Clogging problems in the looped with carrier network are less than those in the traditional looped network, due to the rise in pressures at the drippers which are laid at the end of the laterals (Alabas, 2013). The closed drip network type double inlet, where the best results are in terms of uniformity of distribution and also in the lowest pressure drop, when tested using different lengths of the dripper line and also using different drippers types whether using built-in dripper or the other type is on-line dripper (Tayel et al., 2019). The double inlet and inflow-outflow system achieved better uniformity or dripper flow than that of single inlet systems used for both uniform and non-uniform slope situations. And the maximum pressure difference for the double inlet and inflow-outflow trickle irrigation systems are usually smaller than for single inlet system. The pressure difference of a double inlet or inflow-outflow lateral line system is only about one-third to one-fifth of the pressure difference caused by the single inlet system (Wu and Gitlin, 1982; Nermin, 2007; and Mohanty et al., 2016).

Maize (Zea Mays L.)’s importance is considered one of the main grain crops in Egypt because of it in human, animal and poultry nutrition, as it is used in the manufacture of dry feed at rates of up to 25% of glucose, fructose and oil. Its production in Egypt marketing year 2021/22 (Oct–Sept) at 6.4 million metric tons and the planted area at 800,000 ha (USAD, 2021).

Maize both productivity per hectare and water productivity using drip irrigation system that tended to increase the new cultivated area. Energy savings can be also attained by using drip system to irrigate maize. Drip system can save 33% energy used in irrigation and it can increase energy productivity from 2.81 kg/kW under surface irrigation to 4.98 kg/kW (Ouda et al., 2016). Hussein et al. (2018) studied the effects of full and deficit irrigation and different lateral spacing on corn yield productivity and water use efficiency in sandy soil. He found that preferable lateral spacing for corn plant was found to be 1.20 m, which produced the maximum yield of 11.695 t/ha with the highest water use efficiency (WUE), 1.87 kg/m^3.

This study targeted to select the most suitable closed drip irrigation system design to improve maize yield productivity in the reclaimed lands. The planned design should be distinguished by an efficient hydraulic performance and a better water use efficiency.

2. Materials and Methods

Two field experiments were conducted in two successive seasons (2018 and 2019), at the experimental farm of National Research Centre (NRC), El-Nubaria, Beheira Governorate, Egypt (30.8667 N, 30.1667 E, and main altitude 21 m above sea level). The field experiments was split block design the main plot was irrigation system (surface and sub-surface) and the sub-plots was lateral design (double inlet, loop tube, flushing pipe, and single inlet) with four replicates. The lateral tube of the sub-surface irrigation system was buried at 0.2 m depth.

Four different types of lateral design were tested under surface and subsurface drip irrigation systems. The abbreviations of the four type's lateral designs are listed in Table (1):

Maize (Zea mays L., single cross 10 hybrid) was planted at the second week of May and growing season lasted 120 days. The soil texture was sandy, and its samples were taken every 15 cm from 0 to 60 cm the soil physical analyses are show in Table (2).
Table 1: List of the experimental treatments and its abbreviations.

<table>
<thead>
<tr>
<th>Treatments</th>
<th>Abbreviation</th>
</tr>
</thead>
<tbody>
<tr>
<td>Surface double inlet laterals</td>
<td>(SDI)</td>
</tr>
<tr>
<td>Surface loop tube laterals</td>
<td>(SLT)</td>
</tr>
<tr>
<td>Surface flushing pipe laterals</td>
<td>(SFP)</td>
</tr>
<tr>
<td>Surface single inlet laterals</td>
<td>(SSI)</td>
</tr>
<tr>
<td>Sub-surface double inlet laterals</td>
<td>(SSDI)</td>
</tr>
<tr>
<td>Sub-surface loop tube laterals</td>
<td>(SSLT)</td>
</tr>
<tr>
<td>Sub-surface flushing pipe laterals</td>
<td>(SSFP)</td>
</tr>
<tr>
<td>Sub-surface Single inlet laterals</td>
<td>(SSSI)</td>
</tr>
</tbody>
</table>

Table 2: Physical properties and mechanical analysis of the experimental site soil.

<table>
<thead>
<tr>
<th>Depth (cm)</th>
<th>SP (%)</th>
<th>$\theta_{FC}$ (%)</th>
<th>$\theta_{WP}$ (%)</th>
<th>A.W (g cm$^{-3}$)</th>
<th>BD cm hr$^{-1}$</th>
<th>Course sand</th>
<th>Fine sand</th>
<th>Clay + Silt</th>
<th>Texture</th>
</tr>
</thead>
<tbody>
<tr>
<td>0 – 20</td>
<td>21</td>
<td>10.1</td>
<td>4.7</td>
<td>5.4</td>
<td>1.69</td>
<td>22.5</td>
<td>47.76</td>
<td>49.75</td>
<td>2.49</td>
</tr>
<tr>
<td>20 – 40</td>
<td>19</td>
<td>13.5</td>
<td>5.6</td>
<td>7.9</td>
<td>1.69</td>
<td>19</td>
<td>56.72</td>
<td>39.56</td>
<td>3.72</td>
</tr>
<tr>
<td>40 – 60</td>
<td>22</td>
<td>12.5</td>
<td>4.6</td>
<td>7.9</td>
<td>1.67</td>
<td>21</td>
<td>36.76</td>
<td>59.4</td>
<td>3.84</td>
</tr>
</tbody>
</table>

where: $\theta_{FC}$ = Field Capacity, $\theta_{WP}$ = Wilting Point, A.W = Available Water, BD = Bulk density (g/cm$^3$), and HC = Hydraulic conductivity (cm/hr).

The experimental area was divided into two main plots (surface and sub-surface) and every zone was divided into four sub-plots for lateral designs of 20 × 100 m size. Every sub-plot was divided into four longitudinal quarters, a lateral line was selected at every quarter to determine the pressure drop profile along it, and the measuring point was selected at every 5 meters along the lateral line to measure pressure value and dripper discharge. A schematic plan of the experimental area and types of lateral design are shown in Fig. (1).

Fig. 1: Experiment design of four types of laterals connection to manifolds for surface and sub-surface drip irrigation.
The built-in drippers were tested at the National Irrigation Devices Testing Laboratory of the Agricultural Engineering Research Institute (AEnRI), ARC under 0.5 to 1.25 bar operating pressures for four replicates to determine its actual hydraulic performance.

Irrigation system composed of a control head, valves, and pipeline network, that could be summarized as follows: 1) Control head: It consists of a centrifugal pump 3/3, driven by electric engine (pump discharge of 80 m$^3$/h and 40 m lift), two units of media filter 48", screen filter 2" (120 mesh), back flow prevention device, pressure regulator, pressure gauges, flow-meter, control valves and chemical injection port. 2) Main line: UPVC pipes of 75 mm (ID) to convey the water from the water source to sub-main lines. 3) Sub-main lines: two UPVC pipes of 75 mm (ID) were connected to the main line through a 2" ball valve for both surface and sub-surface zones. Pressure gauges were installed at the start of sub-main lines. 4) Manifolds: every sub-main line was branched into four manifolds UPVC pipes of 50 mm (ID) one for every of experimental treatment sub-units. Manifolds were connected to the sub-main line through control valves 1.5". 5) Lateral lines: PE tubes of 16 mm in (ID) were connected to the manifolds and the laterals have built-in drippers at 0.33m spacing. Laterals were buried under 0.2 m depth from the soil surface of the row in sub-surface drip irrigation treatment as shown in Fig. (2).

![Fig. 2: Lateral position for surface and sub-surface drip irrigation treatments.](image)

2.1. Dripper Hydraulic performance

The relationship between dripper water discharge ($q$) and operating pressure head ($p$) is found as (Clark et al., 2007):

$$ q = k \cdot p^x $$

Where:
- $q$ = Dripper discharge L h$^{-1}$
- $k$ = Dripper discharge coefficient,
- $x$ = Dripper discharge exponent, and
- $p$ = Operating pressure head. bar

2.2. Water distribution uniformity

Emission uniformity, $EU$, is a measure of the uniformity of emissions from all the emission points within an entire trickle irrigation system. For field tests calculated as follows (Killer and Bliesner, 1990):

$$ EU = 100 \frac{q_o}{q_a} $$
Where:
\[ \text{EU} = \text{Field emission uniformity, ~\%} \]
\[ q_{a} = \text{Average dripper discharge in the subunit. L/hr} \]
\[ q_{a} = \text{Average discharge of the drippers on quarter of the area receiving the least amount in the tested subunit, and L/hr} \]

2.3. Yield productivity
The total yield of each treatment as determined using a frame 1m × 1m size. The frame was placed randomly and the maize plants within the frame were weighted.

2.4. Water use efficiency (WUE)
This terminology refers to corn yield per cubic meter of irrigation water. It was calculated according to Israelsen and Hansen (1962) as follows:

\[ \text{WUE} = \frac{Y}{W} \]

2.5. Statistical analysis
All data collected were statistically analyzed as a split plot design with four replications using analysis of variance to evaluate main and interaction effects as described by Snedecor and Cochrane (1982). Means among treatments were compared using Least Difference (LSD) at P 0.05 probability.

3. Results and Discussion

3.1. Dripper Hydraulic performance:
The specifications of actual hydraulic performance of the tested built-in drippers were listed in Table (3).

From the presented data in Table (3) and Fig. (3), it is clear that the relationship between pressure (bar) and dripper flow rate (l/hr) class as (Clark et al., 2007). The dripper flow rate is increased by the increase of operating pressure and the dripper flow rate was 3.6239 l/hr at an operating pressure of 1 bar. The mean values of EU and \( q_{\text{var}} \) was 93 % and 19.5 % which classified as acceptable values, but CV value was 6.98 % which was good according to ASAE standard.

Finally, all drippers were suitable to be installed in the on-field experiments for maize production under aired region conditions.

<table>
<thead>
<tr>
<th>Hydraulic characteristics</th>
<th>Built-in dripper</th>
</tr>
</thead>
<tbody>
<tr>
<td>Flow rate(l/h)</td>
<td>Nominal</td>
</tr>
<tr>
<td>Manufacture's coefficient of variation (CV %) at (1 bar)</td>
<td>Value</td>
</tr>
<tr>
<td>Emission uniformity (Eu %)</td>
<td>Value</td>
</tr>
<tr>
<td>Emitter flow variation (q\text{var} %)</td>
<td>Value</td>
</tr>
<tr>
<td>Turbulent flow regime</td>
<td>Turbulent flow regime</td>
</tr>
<tr>
<td>ASAE standard</td>
<td>Average</td>
</tr>
<tr>
<td>ASAE standard</td>
<td>Excellent</td>
</tr>
<tr>
<td>Classification</td>
<td>Acceptable</td>
</tr>
</tbody>
</table>

Table 3: Hydraulic specifications of built-in dripper.
Fig. 3: The actual hydraulic performance of the built-in drippers.

3.2. Pressure drop

The distribution pressure drop along laterals was differed for every lateral design as presented in Fig. (4). The mean values of maximum pressure drop of the four designs are presented in Table (4). The distribution pressure drop recorded the lowest values at the beginning of laterals for every design but the distribution profile differed according to water flow through the laterals with the inlet connection to the manifold. Results indicated that the lowest pressure drop was recorded for both SSDI and SDI where the lateral connected from both ends to feeding manifolds. The pressure drop percentages were 6.4 and 6.6 % for SSDI and SDI respectively less than operating pressure of the sub-unit. The other closed surface and sub-surface systems recorded a pressure drop percentages of 9.6, 10.3, 9.2, and 8.9 % less than operating pressure of the sub-unit for SLT, SFP, SSLT, and SSFP respectively. The highest pressure drop percentage was recorded to the single inlet design of both surface and sub-surface systems, and it was 12.3 and 9.8 % less than operating pressure of the sub-unit for SSI and SSSI respectively.

It can be noted from the pressure drop distribution profile of both SDI and SSDI that the maximum value of pressure drop was after the middle of the laterals that was due to the flow of water from two manifolds entrance then it meets at the point after the middle of lateral. Accordingly, there was an increase in turbulent flow which increased pressure drop. The opposed water flow existed in the two other closed systems (SLT, SFP, SSLT, and SSFP) at the end of laterals as a result, the maximum values of pressure drop were recorded at the end of laterals due to water energy feedback as higher values.

<table>
<thead>
<tr>
<th>Design</th>
<th>L1</th>
<th>L2</th>
<th>L3</th>
<th>L4</th>
<th>Mean</th>
</tr>
</thead>
<tbody>
<tr>
<td>SDI</td>
<td>0.056</td>
<td>0.074</td>
<td>0.068</td>
<td>0.062</td>
<td>0.065</td>
</tr>
<tr>
<td>SLT</td>
<td>0.093</td>
<td>0.093</td>
<td>0.096</td>
<td>0.095</td>
<td>0.094</td>
</tr>
<tr>
<td>SFP</td>
<td>0.102</td>
<td>0.103</td>
<td>0.101</td>
<td>0.102</td>
<td>0.102</td>
</tr>
<tr>
<td>SSI</td>
<td>0.110</td>
<td>0.120</td>
<td>0.123</td>
<td>0.117</td>
<td>0.117</td>
</tr>
<tr>
<td>SSDI</td>
<td>0.069</td>
<td>0.066</td>
<td>0.053</td>
<td>0.061</td>
<td>0.062</td>
</tr>
<tr>
<td>SSLT</td>
<td>0.091</td>
<td>0.089</td>
<td>0.092</td>
<td>0.092</td>
<td>0.091</td>
</tr>
<tr>
<td>SSFP</td>
<td>0.086</td>
<td>0.089</td>
<td>0.089</td>
<td>0.088</td>
<td>0.088</td>
</tr>
<tr>
<td>SSSI</td>
<td>0.089</td>
<td>0.093</td>
<td>0.098</td>
<td>0.094</td>
<td>0.093</td>
</tr>
</tbody>
</table>
3.3. Emission uniformity

The emission uniformity (EU) for every lateral design was changed with a change in pressure drop as it is shown in Fig. (5). The higher emission uniformity was observed for closed systems comparing the unclosed system. The emission uniformity values were 96.34, 95.67, 93.82, and 91.62 % for SSDI, SSLT, SSFP, and SSSI repetitively for sub-surface drip irrigation system and it were 95.32, 94.49, 92.17, and 90.76 % for SDI, SLT, SFP, and SSI, repetitively under surface drip irrigation system.

The pressure drop variation was lower along the manifolds and also along the individual laterals in closed lateral design compared to the single inlet design. A better pressure distribution throughout
the network was existed, which achieved higher values of emission uniformities as compared to the single inlet type configuration. These results agreed with both (Dhara, 2014; and Mohanty et al., 2016).

![Emission uniformity graph](image1)

**Fig. 5:** Emission uniformity for the four types of lateral design under surface and sub-surface drip irrigation systems.

### 3.4. Yield productivity

The higher yield productivity was produced for the sub-surface than the surface treatments as it can be seen in Fig. (6) due to highest water use by decreasing the water evaporation from soil surface. Also, the closed irrigation systems improved the yield productivity comparing with single inlet treatments. The highest yield produced was about 11.86 t / ha for SSDI treatment where the lowest yield was recorded about 9.07 t / ha for SSI treatment. The other sub-surface drip irrigation treatments produced about 11.57, 10.26, and 9.67 t / ha for SSLT, SSFP, and SSSI respectively. The surface drip irrigation treatments produced about 9.57, 9.38, and 9.07 t / ha for SLT, SFP, and SSI treatments.

The main advantage described for the sub-surface drip irrigation treatments that less irrigation water was applied which is agree with (Wichelns, 2007). The applied irrigation water in the sub-surface drip irrigation systems would not lost by evaporation from the soil surface as it was happened in which improved maize yield productivity. A certain amount of applied irrigation water was lost by evaporation in surface drip irrigation treatments especially under the weather conditions of desert reclaimed lands. The statistical analysis showed that there were significant differences in maize yield at the 5 % probability level and as a result using subsurface drip irrigation system and closed lateral designs treatments as shown in Table (4).

![Maize yield graph](image2)

**Fig. 6:** Maize yield for the four types of lateral design under surface and sub-surface drip irrigation systems.
3.5. Water use efficiency (WUE)

Water use efficiency (WUE) represents a given level of biomass or grain yield per unit of water used by the crop. Results shown in Fig. (7) indicated that the highest WUE was 1.699 kg m$^{-3}$ for SSDI design with an increase 30.8 %, while the WUE of SDI was 1.423 kg m$^{-3}$ with 9.54 % higher comparing SSI which was the lowest WUE (1.299 kg m$^{-3}$). The other closed sub-surface drip irrigation designs were 1.66, and 1.47 kg m$^{-3}$ with a percentage 27.6, and 13.24 % for SSLT, and SSFP, respectively, which were higher than the closed surface drip irrigation designs of 1.372, and 1.344 kg m$^{-3}$ with a percentage 5.62, and 3.46 % for SLT, and SSI, designs respectively.

It is obvious that both the sub-surface drip irrigation and closed lateral designs increased the water use efficiency (WUE) compared to the surface and singe inlet systems. Applying the sub-surface drip irrigation water decreased the loss of irrigation water by evaporation, where the closed drip irrigation systems improved water conveyance efficiency which eliminated or reduced non-productive water use leading to an increase in plant transpiration and yield (Stanhill, 1986). The statistical analysis showed that there were significant differences in WUE at the 5 % probability level and as of result using subsurface drip irrigation system and the closed lateral designs treatments as shown in Table (5).

Finally, results showed that SSDI was the most efficient system design through investigating either in EU, WUE, and yield in comparison with other designs which came after in all measured parameters.

![Water use efficiency for the four types of lateral design under surface and sub-surface drip irrigation systems.](image)

**Fig. 7:** Water use efficiency for the four types of lateral design under surface and sub-surface drip irrigation systems.

**Table 5:** Statistical analyses of emission uniformity, maize yield and WUE under drip irrigation systems and lateral designs treatments.

<table>
<thead>
<tr>
<th>Main effect of treatments</th>
<th>Interaction between treatments</th>
</tr>
</thead>
<tbody>
<tr>
<td>Treatment</td>
<td>EU</td>
</tr>
<tr>
<td>Surface</td>
<td>93.185 b</td>
</tr>
<tr>
<td>Sub-Surface</td>
<td>94.363 a</td>
</tr>
<tr>
<td>DI</td>
<td>95.83 a</td>
</tr>
<tr>
<td>LT</td>
<td>95.08 b</td>
</tr>
<tr>
<td>FP</td>
<td>92.995 c</td>
</tr>
<tr>
<td>SI</td>
<td>91.19 d</td>
</tr>
<tr>
<td></td>
<td></td>
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<td></td>
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</table>

Means with different letters within each column are significant at 5% level.

DI = Double inlet, LT = Loop tube, FP = Flushing pipe, and SI = Single inlet.

4. Conclusion

Field experiments were conducted in two seasons to investigate the effect of the closed designs for surface and sub-surface drip irrigation under maize yield. The lowest pressure drop was recorded for the double inlet design for both sub-surface and surface drip irrigation systems SSDI, SDI that
decrease the pressure drop percentage to 6.4 and 6.6 % respectively. The highest pressure drop percentage was recorded to the single inlet design of surface and sub-surface systems, SSCE, SCE and it was 12.3 and 9.8 % respectively. The highest emission uniformity, crop yield, and water use efficiency were recorded for the double inlet design under sub-surface drip irrigation system 96.34%, 11.86 t / ha, and 1.699 kg m\(^{-3}\) comparing with single inlet design which were 90.76 %, 9.07 t / ha, and 1.344 kg m\(^{-3}\) under surface drip irrigation system, respectively.

The statistical analysis shown a significant differences at the 5% level in both maize yield and water use efficiency between treatments. Generally, Hydraulic performance, Emission uniformity, Crop yield, and Water use efficiency were higher in closed designs SSDI, SDI and sub-surface system comparing with single inlet design and the surface drip irrigation system.

References


